### **Highly Modular TWIN BREAKER Series**

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#### 1. Introduction

The importance of the stable supply of electricity that plays a fundamental role in our contemporary, information oriented society is ever increasing. Electric facilities which supply electric energy must not only be reliable but easy to use, maintainable and flexible to permit specification changes. Manufacturers are developing new technologies for with miniaturization, standardization and automation of electric facilities. With consideration of technical trends and overall cost reduction for electric facilities, we have revolutionalized major component devices such as the molded case circuit breaker and earth leakage breaker. Based on new concepts, Fuji Electric has developed a series of TWIN BREAKERs, the Fuji Auto Breaker (FAB) and Fuji Earth Leakage Breaker (ELB), ranging from 30A to 225A Frames, which have been well received in the market. We have recently developed a series of SUPER TWIN BREAKERs, medium and large-capacity FAB and ELB which range from 400A to 800A Frames, Fuji Electric's TWIN BREAKER series of 30A to 800A Frames is now complete.

### 2. Features of the SUPER TWIN BREAKER

Figure 1 and Figure 2 show an ON/OFF indicator, a TRIP button, a TEST/LEAK indicator button, etc. functionally arranged within window frame on the front cover of the breaker.

Features of the SUPER TWIN BREAKER are described below.

#### (1) FAB and ELB have the same dimensions

Figure 3 shows how we reduced and standardized the number of different frame sizes of our FAB and ELB, 6 different frame sizes for the 400AF to 800AF FAB and ELB have been reduced to 2. The full line of TWIN BREAKERs, ranging from 30A to 800A, has been reduced from 21 frame sizes to only 9. In addition, we developed ELBs which have higher interrupting capacities (Fig. 4), and expanded functions (Fig. 5). As a result, the user can select a breaker with a wider range of ratings, reducing management costs incurred in designing and producing a switch-board.

Fig. 1 400AF SUPER TWIN BREAKER

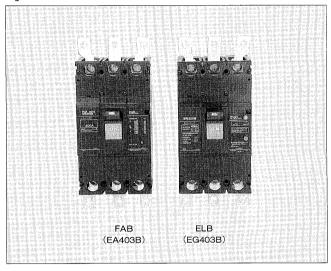
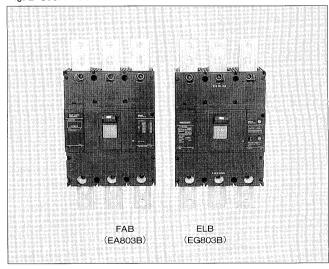


Fig. 2 800AF SUPER TWIN BREAKER



#### (2) Internal accessories in detachable cassette

An internal accessory cassette was constructed to contain such items as an auxiliary switch which outputs the ON/OFF status of a breaker, an alarm switch which outputs the TRIP status, a shunt trip device which trip a breaker

Fig. 3 Reduction of the number of basic frame sizes to nine

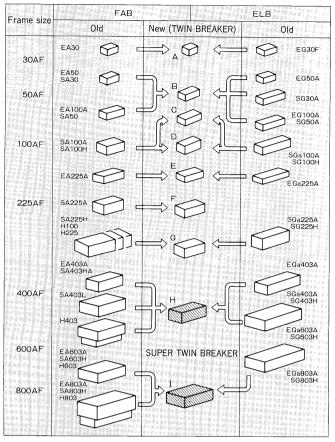
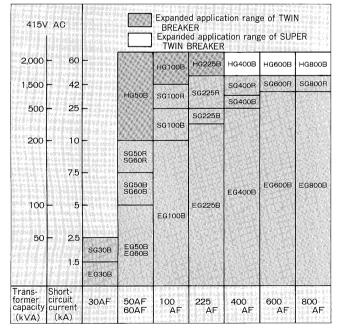
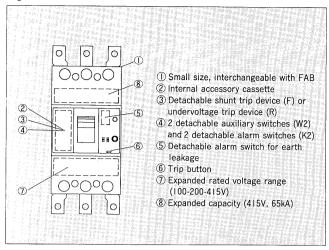


Fig. 4 Expansion of high interrupting capacity ELBs



remotely, and an undervoltage trip device. The user can attach this internal accessory cassette to the front of an already mounted breaker without having to open the cover of that breaker. This internal accessory cassette provides a quick and flexible means to respond to specification

Fig. 5 Enhanced ELB functions



changes which may occur in the course of designing or manufacturing a switchboard, or even after operation has begun.

(3) Breaker is compact and has a high interrupting capacity
Based on Fuji's Active-Arc Driving Technique (AD
technology) which was developed for the TWIN BREAKER, a new compact dual-latch current limiting mechanism
was developed to achieve high current limiting interruption
with large capacity breakers. This has resulted in much
smaller external dimensions, with a maximum 30% volume
reduction for FAB, and about 70% reduction for ELB.
In addition, high-performance ELB models (415V, 65kA)
have been recently developed and added to our product
line.

(4) Conformance with new international standard, IEC 947-2

The TWIN BREAKER (FAB) meets the new international standard for low voltage circuit breakers, IEC 947-2. In the IEC 947-2, the rated service short-breaking (interruping) capacity ( $I_{\rm cs}$ ), specified for assumed operating conditions, is added to the interrupting capacity ( $I_{\rm cu}$ ) which is specified for an assumed fault just beneath the power source transformer. The IEC standard requires an interrupting duty of "O"-"CO"-"CO" for  $I_{\rm cs}$ . The Ics for the TWIN BREAKER (FAB) is 25%  $I_{\rm cu}$  or 50%  $I_{\rm cu}$ .

## 3. Ratings and Specifications of the SUPER TWIN BREAKER

SUPER TWIN BREAKERs have a wide range of different interrupting capacities, enabling economical selection of the main circuit breaker for low voltage utilities. Both the FAB and ELB have economical models (Series E), general purpose models (Series S), and high performance models (Series H). Table 1 and Table 2 show the ratings and specifications of the basic types of SUPER TWIN BREAKERs.

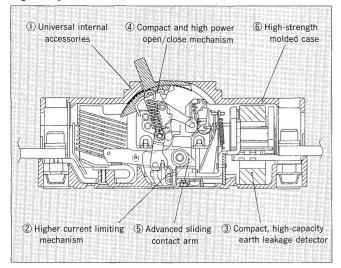
Table 1 Ratings and specifications of SUPER TWIN BREAKERs (FAB)

	Frame (A)			400				600		800		
	Typo	Instantanious tripping current fixed		EA402B			EA403B		EA603B		EA803B	
	Туре	Instantanious tripping current adjustable		EA402BN			EA403BN		EA603BN		EA803BN	
	Rated current (A)			250, 300, 350, 400				500,600		700, 800		
	Poles			2 3			3	-3		3		
es	Rated insulation AC		660					660		660		
series	voltage DC			250				250		250		
E	Rated	500V		18				22		22		
	interrupting capacity (kA) IEC947-2 I <sub>Cu</sub> (sym)	AC	415V	25				35		35		
			240V	35				50		50		
		DC	250V	20				20		20		
	Width		140				210		210			
	Dimensions (mm)		Length	257					275		27	5
	Height			103					103		103	
	Frame (A)				4	00			60	00	80	0
	Туре	Instanta current	nious tripping fixed	SA402B	SA403B	SA40	402R SA403R		SA603R		SA803R	
	Туре	Instantanious tripping current adjustable		SA402BN	SA403BN	SA40	02RN SA403RN		SA603RN		SA803RN	
	Rated current (A)			250, 300,	350,400	00 250.		350, 400	500,600		700, 800	
	Poles		2 3		2		3	3		3		
S.	Rated insulation	AC		660			660		660		660	
series	voltage	DC		250			250		250		250	
S	Rated interrupting capacity (kA) IEC947-2	AC	500V	22			35		`35		35	
			415V	35			50		50		50	
			240V	50			85		85		8	5
	$I_{ m cu}$ (sym)	DC	250V	20			40		40		40	
	Width Dimensions (mm) Length		140			140		210		210		
			257			257		275		275		
	4		Height	10	3		10	93	275		103	
	Frame (A)			400					600		800	
	Tuna	Instantanious tripping current fixed  Instantanious tripping current adjustable		Н402В	H4	03B		H403R	H603B	H603R	Н803В	H803R
	Туре			H402BN	H403BN		I	1403RN	H603BN	H603RN	H803BN	H803RN
	Rated current (A)		250, 300, 350, 400		00	250,3	300,350,400	500,600	500,600	700, 800	700,800	
	Poles		2	3			3	3	3	3	3	
SS	Rated insulation	AC		660				660	660	660	660	660
series	voltage	DC		250				250	250	250	250	250
H	Rated interrupting capacity (kA) IEC947-2 I <sub>cu</sub> (sym)	AC	500V	42				85	42	85	42	85
1			415V	65				125	65	125	65	125
			240V	125				125	125	125	125	125
		DC	250V		40			40	40	40	40	40
			Width	140				140	210	210	210	210
	Dimensions (mm)	ensions (mm) Length Height		257				257	275	275	275	275
				103				103	103	103	103	103

Table 2 Ratings and specifications of SUPER TWIN BREAKERS (FLB)

	Frame (A)			4(	00	600	800	
			High speed type	EG4		EG603B	EG803B	
	lyne		Time delay type	EG40		EG603BD	EG803BD	
	Poles				3	3	3	
	Rated voltage AC (V) High speed type Time delay type		100-200-4			100-200-415 common		
			200-415		200–415 common	200–415 common		
	Rated current (A)		250, 300,		500, 600	700, 800		
			sitive current (mA)	30, 100/200/5		<del></del>	100/200/500 switchable	
les				withi		within 0.1	within 0.1	
series	Rated sens		sitive current (mA)	100/200/50		100/200/500 switchable 100/200/500 switcha		
Ħ	Time delay type Tripping ti			0.3/0.8/2		0.3/0.8/2 switchable	0.3/0.8/2 switchable	
				0.15/0.4/1		0.15/0.4/1 or greater	0.15/0.4/1 or greater	
			AC415V	2		35	35	
	Rated interrupting capacity (sym)		AC200V	3	35		50	
			AC100V	35		50	50	
	Dimensions (mm)		Width	14	10	210	210	
			Length	25	57	275	275	
			Height	10	)3	103	103	
П	Frame (A)			40	00	600	800	
			High speed type			SG603R	SG803R	
	Type		Time delay type	SG403BD	SG403RD	SG603RD	SG803RD	
	Poles			3	3	3	3	
			High speed type	100-200-415 common	100-200-415 common	100-200-415 common	100-200-415 common	
	Rated voltage	e AC (V)	Time delay type	200-415 common	200-415 common	200-415 common	200-415 common	
	Rated current (A)		250, 300, 350, 400	250, 300, 350, 400	500,600	700, 800		
	High speed type  Rated sensitive c  Tripping time (s)		itive current (mA)	30 30, 100/200/500 switchable	30, 100/200/500 switchable	100/200/500 switchable	100/200/500 switchable	
series			me (s)	within 0.1 within 0.1		within 0.1	within 0.1	
			itive current (mA)	100/200/599 switchable 100/200/500 switchable		100/200/500 switchable	100/200/500 switchable	
S				0.3/0.8/2 switchable	0.3/0.8/2 switchable	0.3/0.8/2 switchable	0.3/0.8/2 switchable	
			ng time (s)	0.15/0.4/1 or greater	0.15/0.4/1 or greater	0.15/0.4/1 or greater	0.15/0.4/1 or greater	
			AC415V	30	50	50	50	
	Rated interrupting capacity (sym)		AC200V	42	85	85	85	
			AC100V	42	85	85	85	
			Width	140	140	210	210	
	Dimensions (	mm)	Length	257 257		275	275	
	, ,		Height	103	103	103	103	
	Frame (A)			40	00	600	800	
	High speed type			HG4	·03B	HG603B	HG803B	
	Туре		Time delay type	HG403BD		HG603BD	HG803BD	
	Poles			3 .	3	3		
	Rated voltage AC (V) High speed type Time delay type		High speed type	100-200-4	15 common	100-200-415 common	100-200-415 common	
			200-415	common	200-415 common	200-415 common		
	Rated current (A)		250, 300,	350, 400	500,600	700, 800		
	High speed Rated sensitive current (mA)		30, 100/200/5	00 switchable	100/200/500 switchable	100/200/500 switchable		
series	type Tripping ti		ime (s)	within 0.1		within 0.1	within 0.1	
	Time delay type  Rated sens Tripping ti non-trippin		sitive current (mA)	100/200/50	0 switchable	100/200/500 switchable	100/200/500 switchable	
H			ime (s)	0.3/0.8/2	switchable	0.3/0.8/2 switchable	0.3/0.8/2 switchable	
			ng time (s)	0.15/0.4/1 or greater		0.15/0.4/1 or greater	0.15/0.4/1 or greater	
	Rated interrupting capacity (sym)		AC415V	6	5	65	65	
			AC200V	125		125	125	
1 1			AC100V	12	25	125	125	
			XX 11 1 . 1	140		210	210	
	**************************************		Width	14	+0			
	Dimensions (	(mm)	Length		57	275	275	

Fig. 6 Major technical issues



# 4. Structure and Performance of the SUPER TWIN BREAKER

Figure 6 shows major technical issues which had to be solved to realize the new SUPER TWIN BREAKER. These major issues were (1) to develop an internal accessory cassette which can be mounted after breaker installation, (2) to develop a large capacity and high speed current limiting mechanism, (3) to develop a large capacity and compact earth-leakage-detection unit. In addition, to achieve compact size, it was necessary (4) to develop a compact switching element with large output capacity, (5) to develop a sliding contact arm without a lead wire, and (6) to develop a high strength mold material. All the above were achieved with development based upon Fuji's technology and the use of computer-aided design and simulation.

## 4.1 Internal accessory cassette attachable to an installed breaker

### (1) Need for the internal accessory cassette

More than 30 percent of main circuit breakers are equipped with an auxiliary switch, an alarm switch and internal accessories to send signals such as ON/OFF and TRIP status to, and to receive BREAK signals from a central supervisory facility. This figure, 30%, is almost two times greater than that for branch circuit breakers. The large number of circuit breakers which require internal accessories has led to many variations and combinations of circuit breakers. Previously, as it was necessary to open the circuit breaker cover to mount an internal accessory, the place where this could be performed and the people who could do it were limited. Therefore, it was difficult to respond quickly to specification changes after a switchboard was assembled or operation had begun. The newly developed internal accessory cassette completely solved the above difficulties, enabling any person to mount the accessories easily on any occasion. Even if internal accessories easily on any occasion. Even if internal accessory

Fig. 7 Structure of universal internal accessories

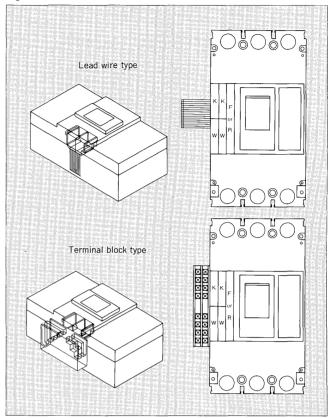
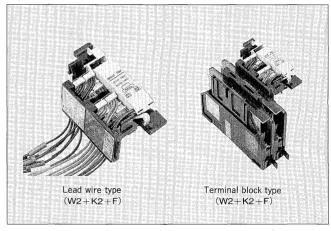


Fig. 8 Internal accessory unit



specifications are not fixed, the user may order a basic breaker unit and proceed to produce a switchboard. When the specification is determined, he has only to attach the specified internal accessory to the breaker. If a facility is in operation, a maintenance person can mount or replace internal accessories whenever electric power is briefly off.

(2) Structure of the internal accessory cassette

Figure 7 shows the internal accessory cassette; in Fig. 8, three accessory elements make up one internal accessory unit; and in Fig. 9, this unit is mounted on a breaker with an auxiliary cover, over the left pole, opened.

(3) Internal accessories are common to all frames

Table 3 shows the available internal accessory units

Fig. 9 Breakers with the same internal accessory unit mounted

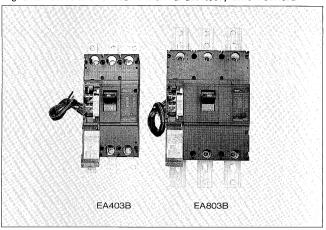


Table 3 Internal accessory combinations for the SUPER TWIN BREAKER

Accessory	Mounting location	Accessory	Mounting location	
Auxiliary switch : W	。 <b>F</b>	W2+R	0	
Alarm switch : K	•	K+F	0	• 04
Shunt trip device : F O		K2+F	* O	
Undervoltage trip : R device O		K+R	0	
W2	00	K2+R	* O	
W+K	0	W+K+F	0	
W2+K	00	W+K+R	0	
K2 **		W2+K+F	0	
W+K2 **		W2+K+R	0	
W2+K2 **	00	W+K2+F	*	•• <b>••</b> ••
W+F		W+K2+R	* O	
W2+F		W2+K2+F	* O	
W+R	0	W2+K2+R	*	

※ : newly available for FAB
○ : newly available for ELB

with different combinations of accessory elements. These units are common to FAB and ELB of 400A to 800A Frames. **Table 3** also shows a shunt trip device and an undervoltage trip device, which were not previously available for ELB. Possible internal accessory variations have increased dramatically.

## 4.2 Realizing high current limiting with a large capacity breaker

(1) Current limiting interruption

The current limiting capability of a low voltage circuit

Fig. 10 Current limiting interruption

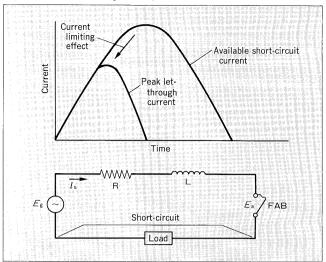
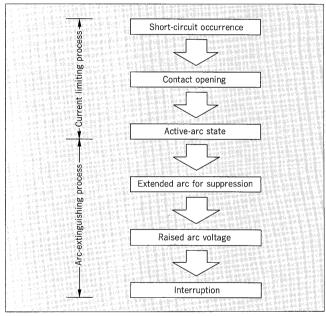


Fig. 11 Interruption process



breaker is determined by how it lowers stress due to arc energy generated during an interruption. Figure 10 shows the principle of current limiting interruption. In this interruption, the electric arc generated between contacts is cooled, arc resistance increased, short circuit current reduced, and then interrupted. Figure 11 shows the interrupting process. To increase the current limiting effect, contacts must open earlier, and move with as high an opening speed as possible, to make the arc change from agglutinative to active states in a very short period of time.

### (2) AD technology for current-limiting interruption

Fuji Electric has already established for TWIN BREAK-ERs of up to 225A Frames, an AD technology that extremely lowers are energy. This technology offers the latest contact-opening method in which the magnetic repulsion force between contacts is concentrated on a current limit-

Fig. 12 Rise-time of arc voltage

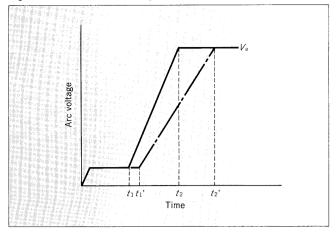
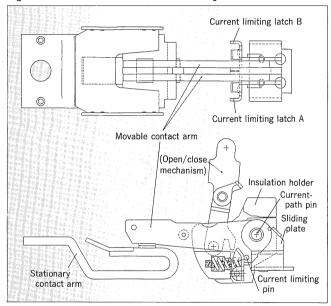


Fig. 13 Sketch of dual-latch current limiting mechanism



ing latch. When the magnetic force exceeds a certain limit this latch is triggered, and the contacts will open quickly.

(3) Applying AD technology to a large capacity circuit breaker

In developing the SUPER TWIN BREAKER, letthrough current and arc power were lowered as much as possible to achieve a compact and high interrupting capacity breaker. Based upon arc voltage data of the TWIN BREAKER (up to 225AF) interrupting a current, a computer was used to simulate the arc voltage when 800Arated contacts interrupt a current. There were a few problems with the above data, shown in Fig. 12.

- (a) Arc agglutination time  $t_1$ ' is longer than  $t_1$  of the small TWIN BREAKER
- (b) Arc rise-time  $t_2$ ' is longer than  $t_2$ .

It was feared that, due to the above, let-through current and arc power might increase so that the internal pressure would exceed the strength of the breaker housing. However, it was found that the contact mass increased to have a larger current capacity. Then, due to an increase in

Fig. 14 Appearance of the dual-latch current limiting mechanism

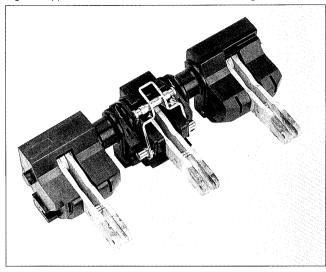
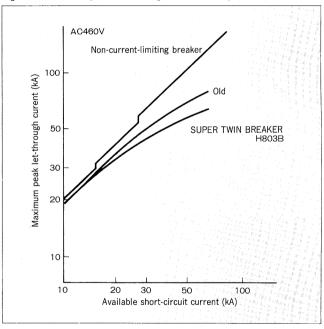


Fig. 15 Maximum peak let-through current comparison



the moment of inertia, the opening speed of the contact decreased.

Figure 13 shows a new device for current-limiting, the dual-latch current limiting mechanism, developed for the SUPER TWIN BREAKER. This mechanism has two movable contact arms, arranged in parallel, each of which has a relatively small mass. The contact arms move independently during early stages of the opening motion, then move jointly until open completely. Figure 14 shows the dual-latch current limiting mechanism. In the past, it has been difficult to obtain current limiting effects with large circuit breakers. The SUPER TWIN BREAKER of 600A and 800A Frames, due to its dual-latch current limiting mechanism, has an arc agglutination time  $(t_1$  in Fig. 12) and an arc rise time  $(t_2$  in Fig. 12) which are as short as those of small circuit breakers. Figure 15 and Figure 16 show current

Fig. 16 Let-through I2 t comparison

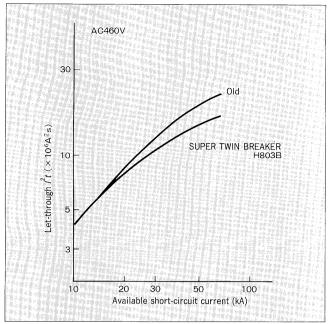
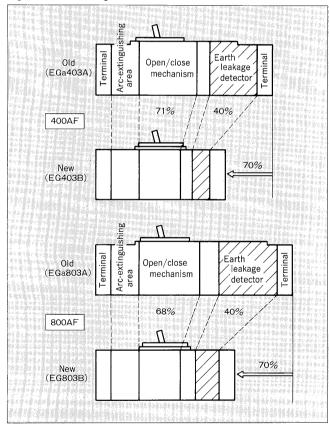


Fig. 17 Miniaturizing of the ELB



limiting characteristics of SUPER TWIN BREAKER H803B at 460V. Both the maximum peak let-through current and let-through  $I^2t$  are extremely low.

## 4.3 Miniaturization of the large capacity earth leakage detection unit

(1) Miniaturization of the ELB

Fig. 18 Comparison of old and new ZCT structures for 800A Frame ELB

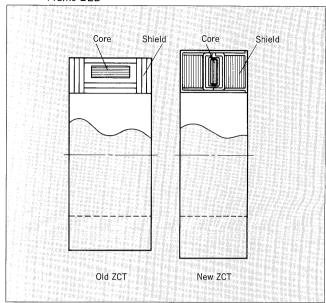


Fig. 19 Equilibrium characteristics of the 800A Frame ZCT

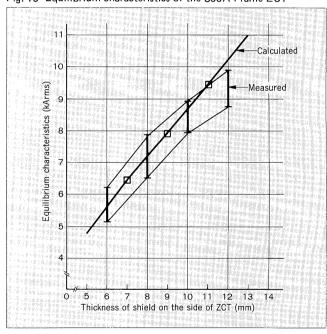
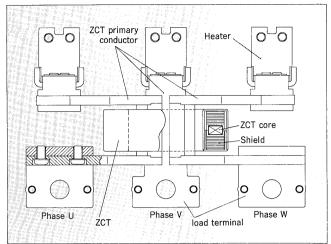


Figure 17 compares the size of the SUPER TWIN BREAKER (ELB) and the old ELB. Both 400A and 800A Frame models decreased to 70% of their previous length. The miniaturization of the compact switching mechanism and earth leakage detection unit was difficult because these parts included terminals and current-breaking parts which were difficult to make compact. It was necessary to reduce the earth leakage detection unit to 40% of its previous size. This was achieved through the optimum construction of a zero-phase current transformer (ZCT) and its primary conductor which usually occupy most of the space in an earth leakage detection unit.

Fig. 20 Structure of the new 800A Frame ZCT and primary conductor



### (2) Flattening the ZCT's core

Basic ZCT characteristics include zero-phase current detection and equilibrium characteristics. The former is explicitly determined by the ELB sensing current and ZCT core volume. The latter characteristic relates to the level of load current which does not cause the ZCT to output. This characteristic is expressed in multiples of the rated current. Optimum core shielding determines ZCT dimensions for large capacity ELB. This is because the ZCT

primary conductor generates a leakage flux which passes through core, and causes the ZCT to output. Figure 18 compares the construction of ZCT for old and new ELB of 800A Frames. The thickness of the ZCT laminated core for new ELB's has been minimized, and a shield has been placed on both sides of the core. As a result, the effect of leakage flux from the primary conductor, which is placed in a hole on the ZCT, is reduced leakage flux from a part of the primary conductor positioned on the side of the ZCT is effectively shielded.

The magnetic field was analyzed, and equilibrium characteristic measured. As Fig. 19 shows, both the calculated and measured characteristics were in agreement. From the above, an optimum thickness for the ZCT core was determined. Figure 20 shows the new 800A Frame ZCT and primary conductor.

#### 5. Conclusion

In addition to 30A to 225A Frame TWIN BREAKERs, Fuji Electric is marketing the SUPER TWIN BREAKER introduced in this article. Dimensions have been standardized for FAB and ELB of identical frames (ranging from 30A to 800A Frames). Fuji Electric's TWIN BREAKER product line is now complete. We are confident that this TWIN BREAKER product line with its compact size, high performance and high flexibility is sufficient for the needs of advanced and complex electric facilities.